

Large-Area and Flexible Lead-Free Nanocomposite Generator Using Alkaline Niobate Particles and Metal Nanorod Filler

Chang Kyu Jeong, Kwi-Il Park, Jungho Ryu, Geon-Tae Hwang, and Keon Jae Lee*

The lead-free nanocomposite generator device for high-output energy harvesting using piezoelectric alkaline niobate-based particles (KNLN) and copper (Cu) nanorods filler is reported. To produce the piezoelectric nanocomposite (p-NC), lead-free KNLN particles synthesized using a solid-state method and the Cu nanorods are distributed in a polydimethylsiloxane (PDMS) matrix. The lead-free flexible nanocomposite generator (NCG) made by a simple spin-casting method successfully converts mechanical energy to electricity up to 12 V and 1.2 μ A. These are higher than previously reported outputs from other lead-free and composite-based nanogenerators. The harvested energy is utilized to directly turn on white light emitting diodes (LEDs) without external circuits and to operate a complex circuit liquid crystal display (LCD). A large-area NCG device (30 cm \times 30 cm) is also fabricated using the bar-coating method to obtain maximum output up to 140 V and 8 μ A (\approx 0.5 mW). This NCG technology has substantial advantages as a simple, cost-effective, scalable, and high-throughput approach for practical flexible electronics, bio-eco-compatible self-powered systems, and body sensor networks (BSN).

BaTiO₃ nanoparticles (BTO NPs) and graphitic carbon nanomaterials, was reported by our group to provide cost-effective and flexible energy harvesting systems for self-powered nano/micro-devices.^[8] However, the previous NCG device had critical drawbacks to be resolved such as low piezoelectric properties of BTO NPs and aggregation of graphitic carbon nanomaterials.

Among the various lead-free perovskite materials with high piezoelectricity, such as Ba(Zr, Ti)O₃ (BZT),^[9] (Bi, Nd) Ti₃O₁₂,^[10] SrBi₂Ta₂O₉,^[11] and (K, Na)NbO₃ (KNN),^[12] KNN-based alkaline niobate is the most attractive lead-free piezoelectric materials due to its remarkable piezoelectric properties, biocompatibility, high Curie temperature, and large electromechanical coupling factor.^[13,14] Especially, KNN-based materials modified by doping elements can have noteworthy piezoelectric coefficients (d_{ij}) (>300 pC N⁻¹),^[13,15] compared to BTO,^[16] KNbO₃,^[17] NaNbO₃,^[18] or pure KNN^[19,20] (<100 pC N⁻¹). In particular, a specific alkaline niobate-based materials of outstanding piezoelectricity ($d_{33} \approx 310$ pC N⁻¹) was reported with the nominal composition of 0.942(K_{0.480}Na_{0.535})NbO₃-0.058LiNbO₃ (KNLN).^[21,22] In addition to piezoelectric material properties, to achieve a high-output nanocomposite generator, good dispersity of piezoelectric particles is also very important for well-distributed piezopotential within an active energy harvesting composite layer. For uniform dispersion, metal nanowires and nanorods are considered more suitable for nanocomposite systems than the previous carbon-based nanofillers of BTO-based NCG, due to the weak van der Waals self-interactions of metal nanomaterials.^[23]

Herein, we demonstrate a high-performance, lead-free NCG device using the intrinsically excellent piezoelectric KNLN particles and well-dispersed copper nanorods (Cu NRs). The KNLN particles as power generation sources and Cu NRs as energy enhancers are embedded in a polydimethylsiloxane (PDMS) elastomeric matrix to construct a piezoelectric nanocomposite (p-NC). The roles of the Cu NRs in the p-NC are dispersing, reinforcing, and conducting agents for the high-output NCG device. The spin-casted p-NC layer is placed between two dissimilar indium tin oxide (ITO)-deposited polyethylene terephthalate (PET) flexible substrates. During periodical

1. Introduction

Energy harvesting using mechanical energy sources (e.g., human walking, transportation movement, and even sound waves) is a promising candidate for energy generation with improved accessibility and eco-compatibility.^[1–3] Since the first nanogenerators were demonstrated for direct energy conversion from mechanical motion to electrical power,^[4] the development of milliwatt (mW)-scale piezoelectric nanogenerator has been attempted to establish wireless communication-sensor networks and self-powered flexible electronics in biological and environmental monitoring systems.^[1,5–7] Recently, a flexible nanocomposite generator (NCG), using perovskite piezoelectric

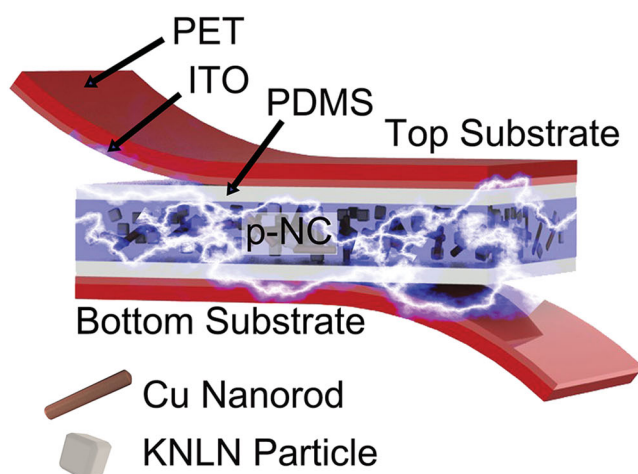
C. K. Jeong, K.-I. Park, G.-T. Hwang, Prof. K. J. Lee
Department of Materials Science and Engineering
Korea Advanced Institute of Science and Technology (KAIST)
291 Daehak-ro, Yuseong-gu
Daejeon, 305–701, Republic of Korea
E-mail: keonlee@kaist.ac.kr

Dr. J. Ryu
Functional Ceramics Group
Korea Institute of Materials Science (KIMS)
797 Changwondaero, Seongsan-gu,
Changwon, Gyeongnam, 642–831, Republic of Korea



DOI: 10.1002/adfm.201303484

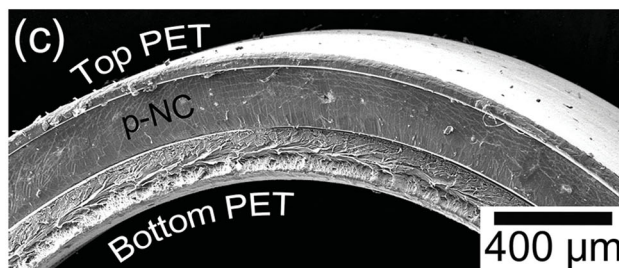
(a) KNLN-based NCG Device



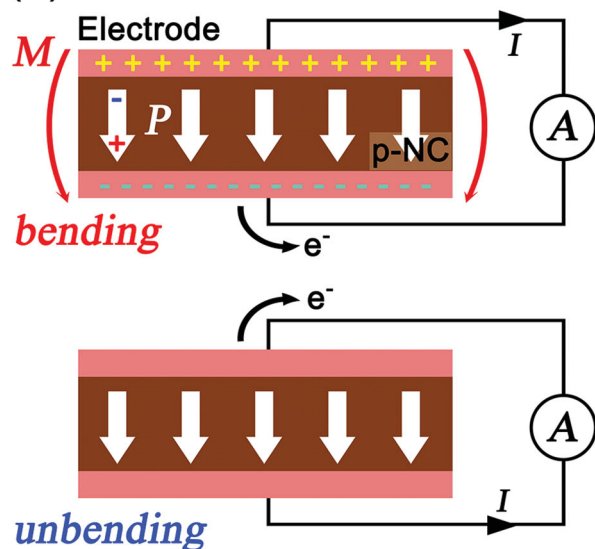
(b)



(c)



(d)



(e)

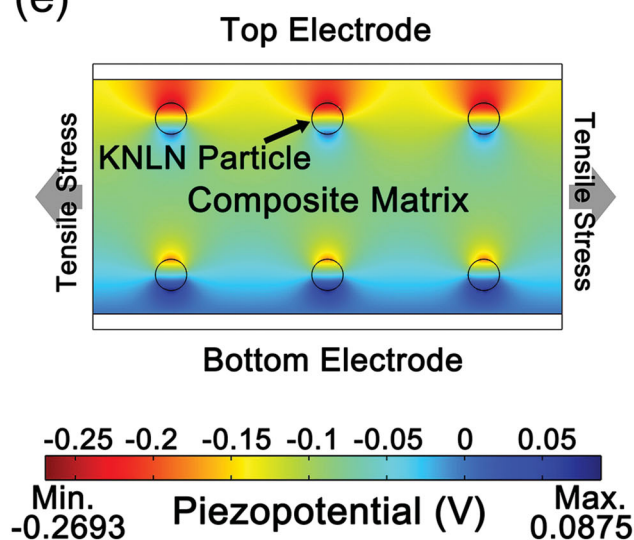


Figure 1. a) Schematic of an NCG device using KNLN particles and Cu NRs. b) Photograph of the flexible p-NC layer attached to a rolled paper. The inset shows the final NCG device bent by fingers. c) Cross-sectional SEM image of a bent KNLN-based NCG. d) Schematics showing the power generation mechanism of the NCG device. In the bending state, the current flow is generated from top to the bottom electrode due to the positive piezoelectric potential induced on the top side. In the unbending state, the accumulated charges return to the original state due to piezopotential vanishment which causes output signals in the opposite direction. e) Simulation result of generated piezopotential distribution inside a p-NC layer of well-dispersed KNLN particles, when a tensile strain of 0.33% is applied by bending.

bending deformation, the KNLN-based flexible NCG device (3 cm × 3 cm) produced maximum electrical signals of ≈12 V and ≈1.2 μA, which are four times higher than those of a previous lead-free BTO/carbon nanotube (CNT)-based NCG device. The electrical energy is utilized to directly turn on white light emitting diodes (LEDs) without external circuits and to operate a complex circuit liquid crystal display (LCD). Furthermore, a large-area NCG device (30 cm × 30 cm) by the bar-coating method can convert the biomechanical energy to sub-mW level power (140 V and 8 μA).

2. Results and Discussion

Figure 1a presents the schematic of the NCG structure with KNLN particles and Cu NRs, which construct a well-distributed p-NC layer in the device. The two ITO electrodes on the flexible PET substrate act as a current collector in the NCG device. The pure PDMS dielectric layers are used to prevent electrical breakdown during the high voltage poling process and extreme mechanical deformation. A flexible p-NC film can be completely attached to a curved surface, as shown in Figure 1b,

and is placed between the different top and bottom ITO-deposited PET substrates for the bendable NCG device (inset of Figure 1b). Figure 1c shows the cross-sectional SEM image of a bent KNLN-based NCG device made of a p-NC (thickness in 250 μm) which is sandwiched between the two flexible substrates. Despite the mechanical deformation, there is no separation of the p-NC layer and plastic substrates owing to the inherent stickiness of the PDMS. The process of energy generation from the NCG device is illustrated in Figure 1d, which shows that KNLN particles harvest external mechanical energy to make electrical potential. Typically, the perovskite KNN-based piezoceramics have orthorhombic or tetragonal crystalline symmetry, with monoclinic subcell structure at around Curie temperature.^[24] When the NCG is subject to external bending force, piezoelectric potential is generated between the two electrodes due to the mechanical stress induced in the aligned dipoles of the embedded KNLN particles. These positive and negative piezopotentials make an instantaneous built-in potential in the external circuit, which drives the current flow (top panel of Figure 1d). During the subsequently unbending of the NCG device, the mechanical stress and piezoelectric potential disappear, which can cause reverse electrical signals (bottom panel of Figure 1d). A simulation for the induced piezopotential in mechanically stressed KNLN-based NCG is also performed via a finite element method (FEM) with six KNLN particles well-dispersed in a PDMS elastomeric matrix, which is conducted by using COMSOL multiphysics software, as described in Figure 1e. The p-NC layer in the NCG suffers tensile stress during bending deformation because the p-NC is placed above the mechanically neutral region. Differences in the piezoelectric potential are illustrated by color code, when a tensile strain of 0.33% is applied to the p-NC layer along the x-axis. The simulated piezopotential distribution in the KNLN-based p-NC is higher than that of BTO NPs embedded p-NC, due to the high electromechanical coupling factor (k) of KNLN caused by its low permittivity (dielectric constant, ϵ) and large d_{33} . The value of k indicates the effectiveness of conversion between mechanical and electrical energy, and can be expressed as follow

$$k^2 = Y \times g_{ij} \times d_{ij} = Y \times \frac{d_{ij}^2}{\epsilon T} \quad (1)$$

where Y , g_{ij} , and ϵ^T are the Young's modulus, piezoelectric voltage constant, and permittivity at constant strain.^[25,26] The physical properties of KNLN established in previous theoretical reports are applied in this simulation.^[19,21,27–30] Based on the results from this FEM-based simulation, the KNLN particles-based NCG device can be expected to generate high electrical outputs from mechanical stress, compared to previous BTO-based NCG.^[8]

The highly piezoelectric KNLN particles used in this study are fabricated by the solid-state synthesis method (see Experimental Section). Scanning electron microscopy (SEM), X-ray diffraction (XRD), and Raman spectroscopy are utilized to characterize the KNLN particles. Figure 2a is an SEM image of the KNLN particles which have polydisperse angulated shapes of 1 to 3 μm . The XRD patterns of the as-synthesized KNLN (inset of Figure 2a) correspond well to those of general perovskite KNN-based materials.^[24] The XRD peaks indicate the tetragonal phase of KNLN due to the near-singlet at 32° (blue arrow) and

the high-back doublets at 22°, 46°, 51°, and 57° (see Figure S1 in the Supporting Information for the magnified XRD pattern of the red-dotted border). In the Raman spectrum of KNLN particles (Figure 2b), the main vibration modes associated with the perovskite crystal structure are shown. The A_{1g} (ν_1) and F_{2g} (ν_5) Raman modes, in particular, are strongly detected as well-known phenomena in KNN-based materials.^[15] Moreover, the weak E_g (ν_2) shoulder at 560 cm^{-1} and the small mound in the 400 to 500 cm^{-1} region prove the tetragonal phase of the KNLN particles.^[31] These XRD and Raman spectroscopy results indicate that the synthesized KNLN particles have a perovskite crystalline structure and ferroelectric tetragonal phase. The crystal structure of the KNLN particles is also investigated by high resolution transmission electron microscopy (HRTEM), as shown in Figure 2c. The diffraction pattern through the fast-Fourier transform (FFT) analysis indicates a single crystal structure (inset of Figure 2c). The interplanar distance displayed in the HRTEM image corresponds to the (010) and (100) crystal planes; which have lattice parameters of $a = b$ in tetragonal symmetry.^[32] The Cu NRs (Sky Spring Nanomaterials, Inc.), which have a diameter of 200 to 400 nm and a length of $\approx 5 \mu\text{m}$ (Figure 2d), show XRD patterns of good crystallinity with very few tenorite (CuO) peaks of (inset of Figure 2d). Figure 2e displays an SEM micrograph of mixed nanomaterials with KNLN particles and Cu NRs. A magnified cross-sectional SEM image of the p-NC (Figure 2f) also shows that the KNLN particles and Cu NRs are well-dispersed in the elastomeric matrix. These images verify that good dispersity of the KNLN particles and Cu NRs is maintained before and after mixing with the PDMS elastomeric matrix.

To measure the electrical signals from the NCG device, a source-meter (Keithley 2612A), a linear motor, and a Faraday cage are used in this work. During the mechanical bending deformation, the uniform voltage and current outputs are generated from the lead-free KNN-based NCG device (Figure 3a,b). The open-circuit voltage and short-circuit current by the NCG device are about 12 V and 1.2 μA , respectively. These output signals are the highest output recorded among those of previously reported flexible and lead-free composite-based nanogenerators.^[8,17,18,33–35] To confirm the measured electrical signals from piezoelectric outputs of the NCG device, a switching polarity test has been performed. When the measurement unit has a forward connection with the KNLN-based NCG device (Figure 3a–i), positive pulses are measured during the bending motions (Figure 3a–ii,a–iii). Under the reverse connection (Figure 3b–i), on the other hand, negative peaks are generated in the bending states of NCG device (Figure 3b–ii,b–iii). Furthermore, we have conducted a linear superposition test which shows the merged output voltage (Figure 3c) and current (Figure 3d) by connecting the two different NCG devices in series and in parallel, respectively. From these results, the generated signals can be verified as electrical outputs by the mechanically stressed KNLN-based p-NC in the NCG devices.

Figure 4a presents the output voltages generated from the devices fabricated using only a PDMS layer (i), a Cu NRs-PDMS composite (ii), a composite with only KNLN particles (iii), and an NCG device (iv). As shown in Figure 4a–i,a–ii, there is no reliable signal from devices containing only a pure PDMS layer, or from Cu NRs embedded in a PDMS layer. Some low electrical signals from these two devices without KNLN particles are

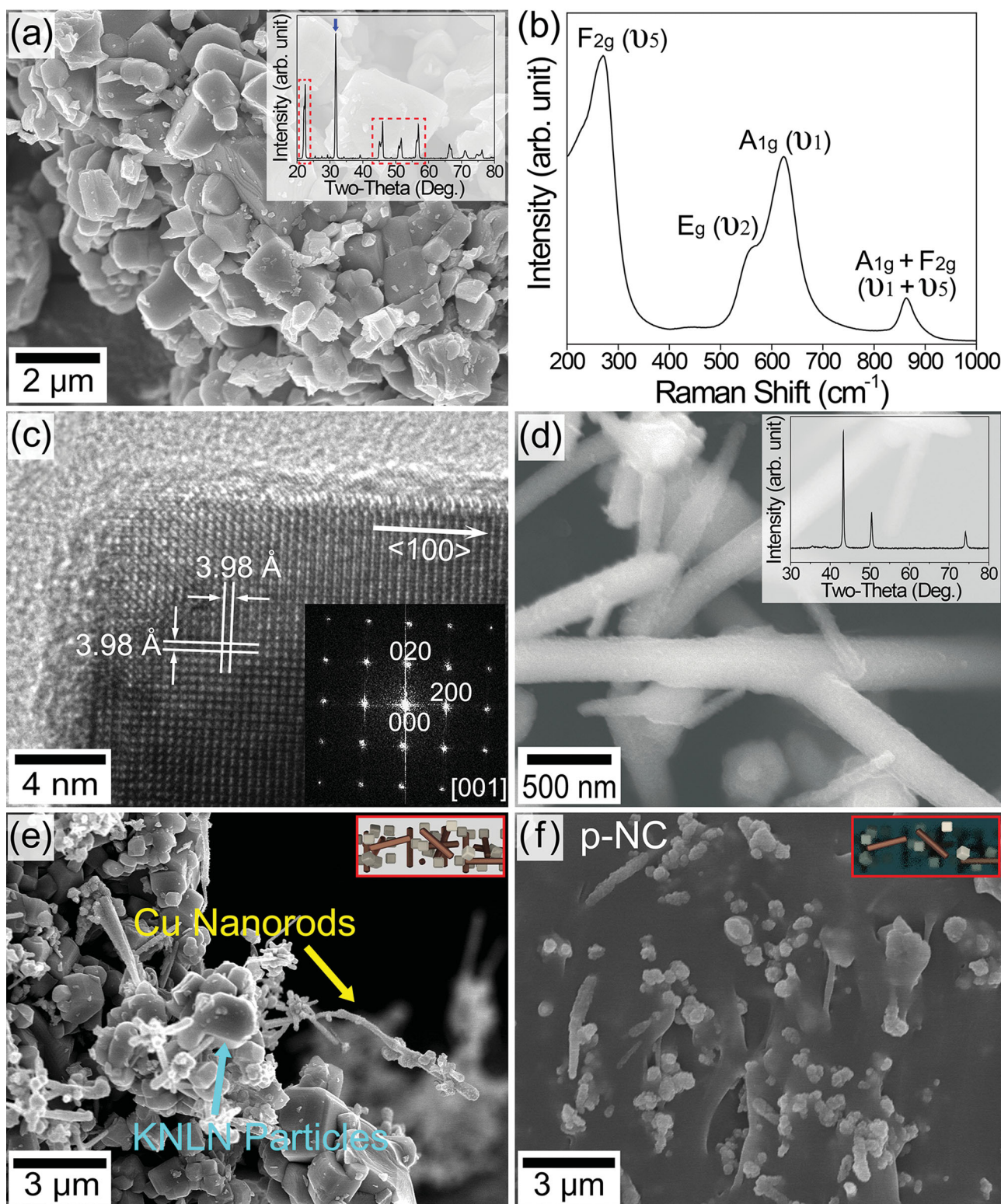


Figure 2. a) SEM image of the KNLN particles synthesized by a solid-state reaction. The inset shows XRD patterns of the KNLN particles. b) Raman spectra of the KNLN particles which presents perovskite crystalline structure of the tetragonal phase. c) HRTEM image and diffraction spots through FFT analysis (inset) from an individual KNLN particle. d) SEM micrograph and XRD peaks (inset) of Cu NRs having a diameter of 200 to 400 nm and a length of $\approx 5 \mu\text{m}$. e) Magnified SEM images of the mixed nanomaterials composed by of KNLN particles and Cu NRs before PDMS blending. f) SEM micrograph of the cross-sectional piezoelectric nanocomposite (p-NC) with PDMS matrix.

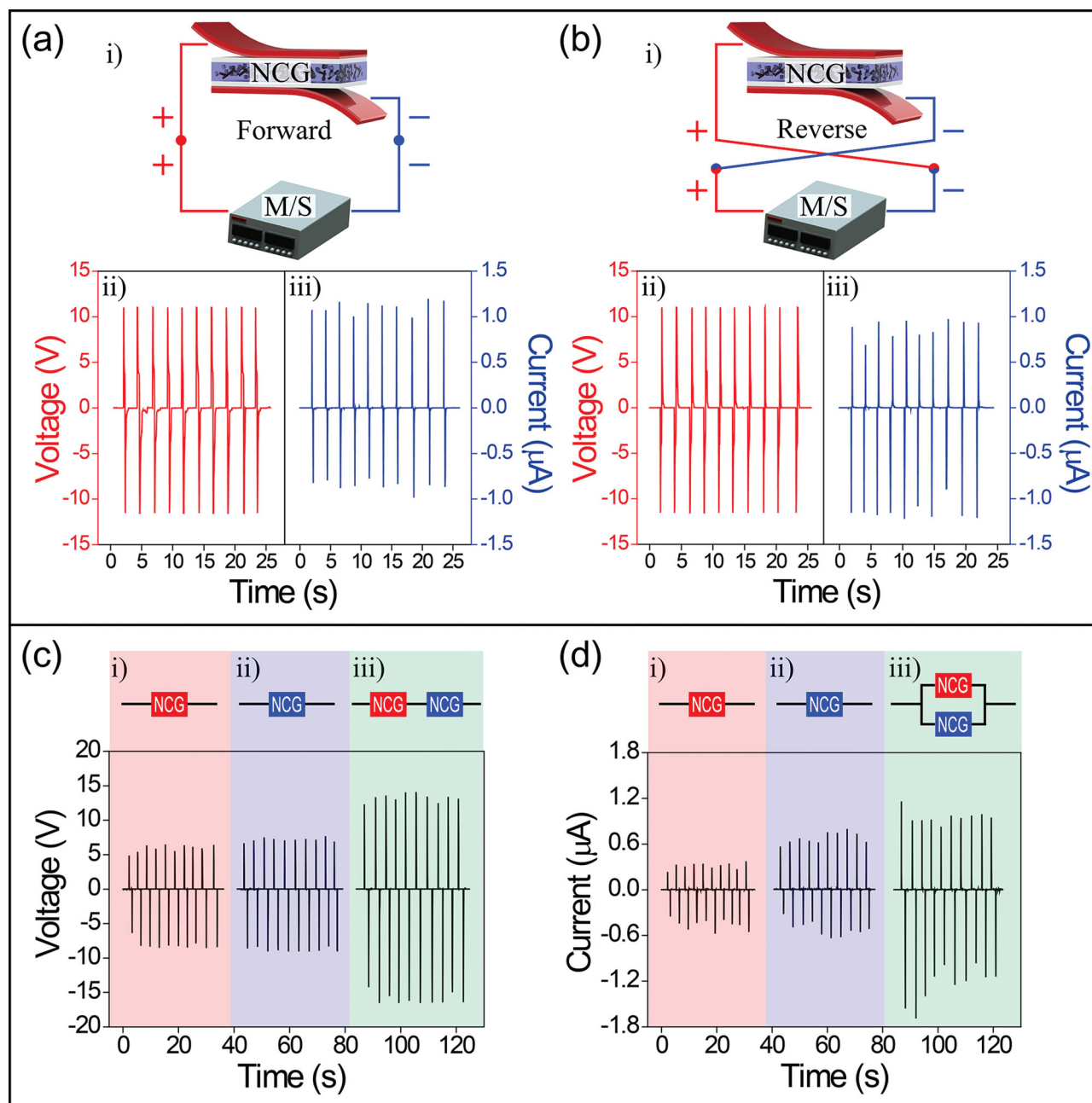


Figure 3. a) During deformation of the NCG device by bending and unbending, the measured outputs of open-circuit voltage and short-circuit current signals when the measurement unit is forward-connected. b) Results of the switching polarity test performed to confirm that the measured electrical signals are produced by the piezoelectric effect of the NCG device. Under the reverse connection, the polarities of voltage and current signals are inverted. c) The output voltage and d) current signals are merged by connecting the two different NCG devices in serial and parallel connection, respectively.

presumably caused by several electrostatic charges at the electrodes. However, this effect can be ignored in comparison to the robust piezoelectric effect by the KNLN particles. From these control experiments, it is clear that the high-output signals of the NCG device are contributed by neither triboelectric effects nor surface charges. Although the PDMS-KNLN composite-based nanogenerator can produce sharp electrical signals (Figure 4a–iii), the output peaks are much lower than those of NCG devices with both KNLN particles and Cu NRs (Figure 4a–iv)

owing to the absence of dispersing and reinforcing agents. Moreover, the Cu NRs filler in the p-NC can play the role of nano-electrical bridges which lead to short voltage lifetimes for higher output performance.^[8,34] Figure S2 and Table S1 of Supporting Information show that the NCG device generates voltage signals whose voltage lifetime is shorter than that of the device without the Cu NRs filler. The measured output current signals also show behavior similar to that mentioned above (Figure S3, Supporting Information). Moreover, we have

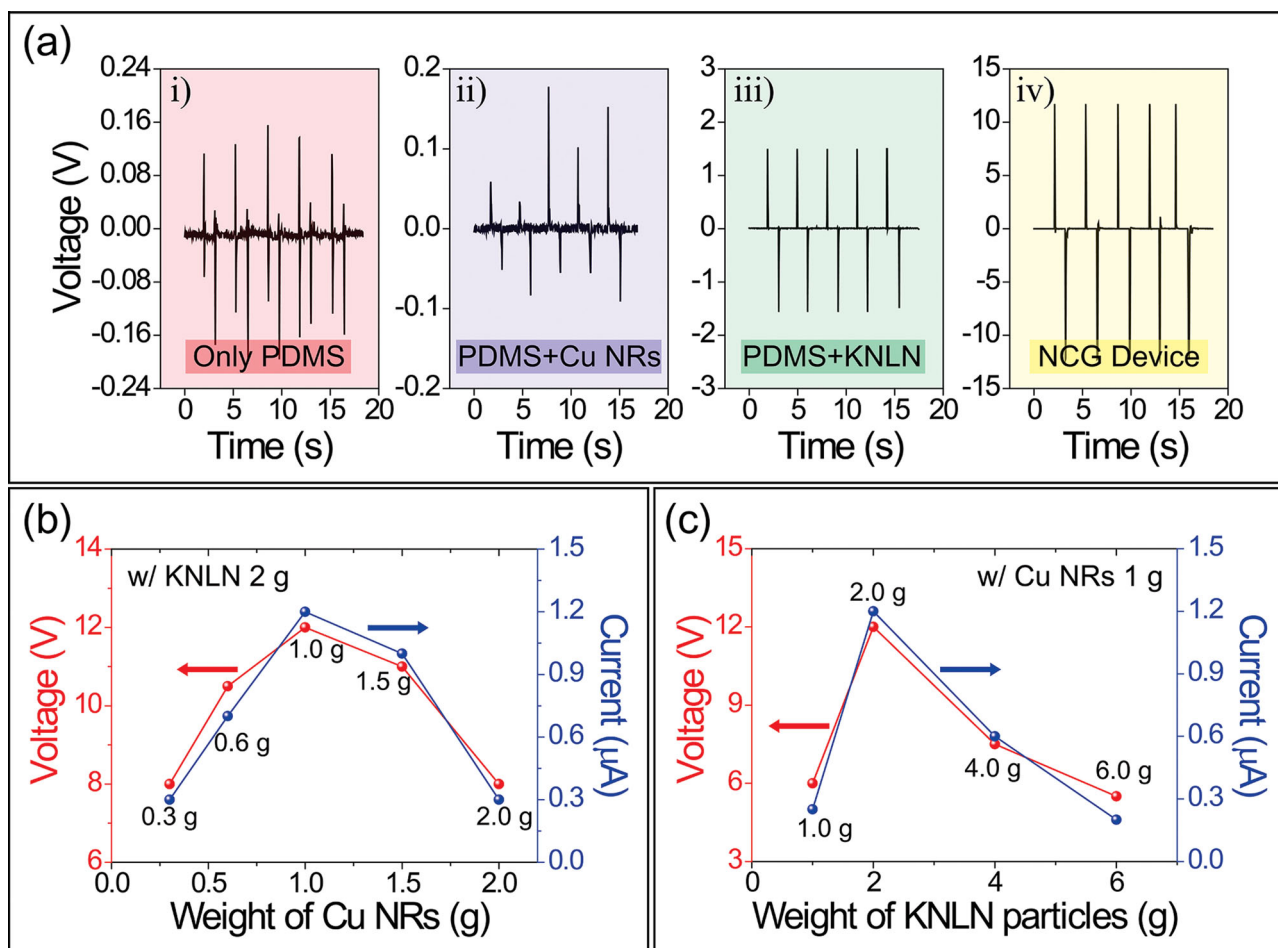


Figure 4. a) Output voltage generated from the devices fabricated using only a PDMS layer (i), a Cu NRs-PDMS composite (ii), a composite with only KNLN particles (iii), and an NCG device (iv). b) Variation of output voltage and current produced from NCG devices with the different weights of Cu NRs at the fixed weight of KNLN particles. c) Generated output signals of NCG devices with various weights of KNLN particles at the fixed amount of Cu NRs.

measured electrical outputs from a KNLN-based NCG device with multi-walled CNTs (MW-CNTs), which have roles similar to those of Cu NRs in an NCG device (Figure S4, Supporting Information). The signals generated from an NCG device using MW-CNTs are lower than those of the NCG device with Cu NRs filler because MW-CNTs are easily aggregated and bundled compared to Cu NRs, as shown in Figure S5 (Supporting Information). It is presumably due to the large van der Waals forces of MW-CNTs caused by π - π stacking interactions^[36–38] that can induce aggregation. The NCG device using Cu nanoparticles (Cu NPs) as nanofillers generates low output signals since the low aspect ratio cannot contribute the dispersity of p-NC, as shown in Figure S6 (Supporting Information).

To determine an optimal composition of the p-NC for effective energy harvesting, NCG devices with various mixture ratios are fabricated with different amounts of KNLN particles and Cu NRs (in 10 g of PDMS matrix). As shown in Figure 4b, the output voltage and current signals from deformed NCG devices rise with increasing amounts of Cu NRs, up to 1 g at the fixed weight (2 g) of KNLN particles, since the Cu NRs filler functions as the dispersing, reinforcing, and conducting agent.

When the Cu NRs amount is above 1 g, the electrical output signals decline with increasing concentration of Cu NRs, due to leakage charge flows within the p-NC caused by weakened insulation of the polymeric matrix. When the amount of KNLN particles is varied (Figure 4c), the generated outputs of NCG devices increase initially with the weight of KNLN particles (fixed Cu NRs weight of 1 g) due to the increment of piezoelectric particle density in the p-NC. Moreover, Maxwell-Wagner-Sillars polarization, which introduces a dramatic change of the overall dielectric constant in composites,^[39,40] can rise with increasing amount of KNLN particles. This leads to extensive polarization which results in high output signals. However, an excessive amount of KNLN particles (above 2 g) in the p-NC lowers the electrical outputs from NCG devices because of the degraded electromechanical coupling effect resulting from an overly-high dielectric constant of the entire p-NC, as expressed by Equation 1. In addition, the large quantity of piezoceramic elements in a composite also can yield the electrical breakdown, resulting in low generated outputs.^[35]

The poling process is necessary to align the piezoelectric dipoles in the KNLN particles along an identical direction to

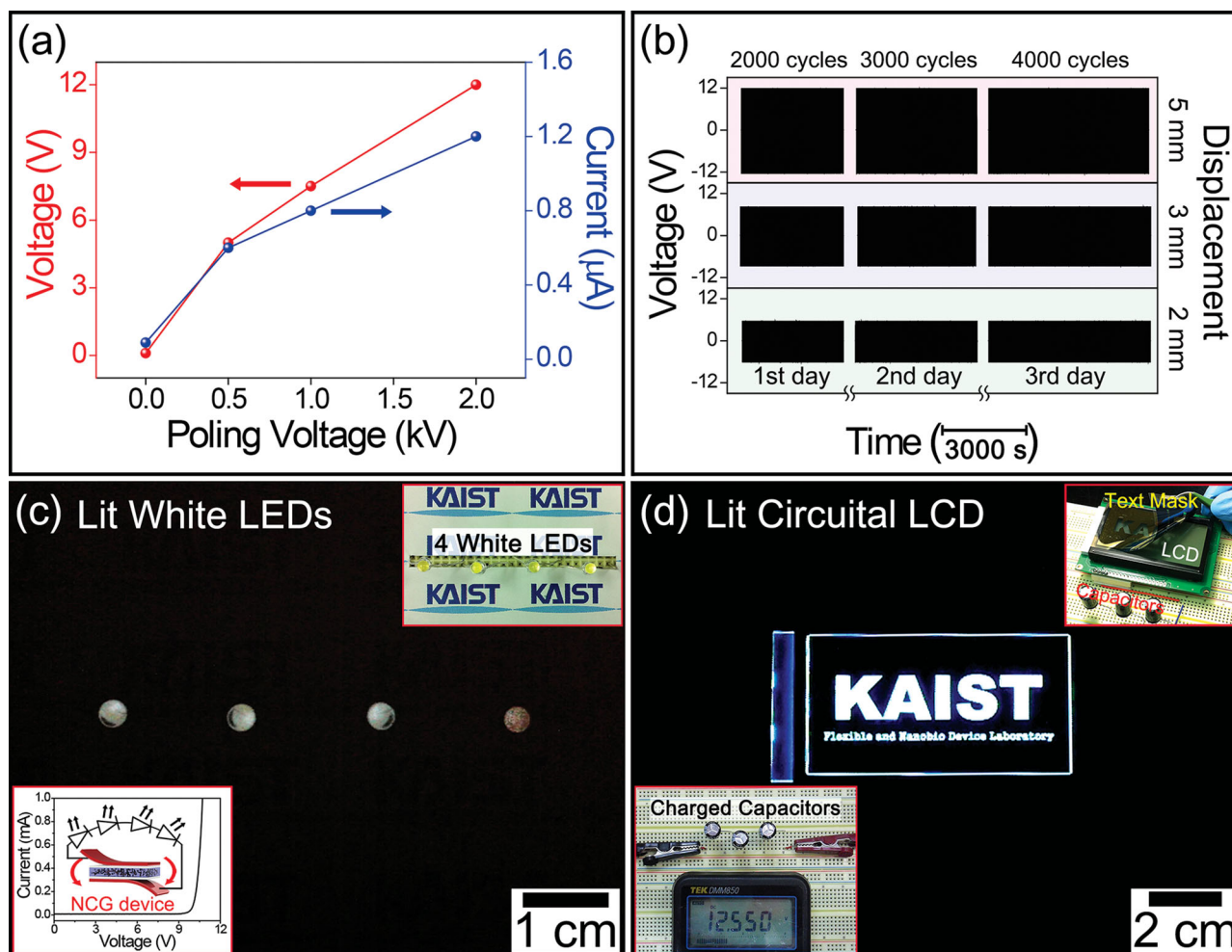


Figure 5. a) Output voltage and current generated from the NCG device as a function of poling voltage from 0 (non-poling) to 2 kV. Output signals gradually rise with increasing poling voltage. b) The strain-dependent property and mechanical durability of the KNLN-based NCG device. The measured voltage signals of each device under different angular strain are stably maintained for three days with different cycles. c) A snapshot taken from the four white LEDs (top inset) driven by the NCG device without external electricity or circuits. The bottom inset shows the current-voltage curve of the four white LEDs aligned in series. The turn-on voltage of the four LEDs in serial connection is about 10.5 V. d) A captured digital photograph of a commercial LCD device operated by the capacitors charged by the NCG device (bottom inset). The top inset shows an LCD device connected in a circuit board with a text mask.

improve the energy harvesting of the NCG devices. **Figure 5a** presents the generated output voltage and current signals from the KNLN-based NCG devices polarized by various levels of external poling voltage from 0 to 2 kV. The low electrical outputs from a non-poled NCG device increases to about 12 V and 1.2 μA when the device is poled at 150 °C under 2 kV. **Figure 5b** displays the strain-dependent property and mechanical durability of the KNLN-based NCG device. The higher angular bending strain (larger displacement) induce higher electrical outputs from the NCG device. Additionally, the measured voltage signals in different strains (2, 3, and 5 mm of displacement) are stably maintained for three days with different numbers of cycles (2000, 3000, and 4000 cycles). This outstanding stability of an NCG device is attributed to the flexible and robust characteristics of the composite layer under mechanical deformation. The generated outputs of the NCG

device, at different frequencies and strain rates, are also measured (**Figure S7**, Supporting Information).

We have applied the power generated by the NCG to operating two commercial electronic units. The top inset of **Figure 5c** is a photograph of the white LEDs array connected with the KNLN-based NCG device. During bending deformation of the NCG device, the four white LEDs are driven by the generated output voltage (**Figure 5c**) without external capacitors or batteries. The LEDs are simultaneously operated at various frequencies of bending and unbending deformation (see Supporting Information, Video S1). To store the electrical energy from the deformed KNLN-based NCG device, we use four diodes as a bridge rectifier circuit, and three 1 mF capacitors connected in parallel. The saturated voltage of ≈4.18 V is provided to each capacitor by the repeated bending/unbending deformation of the NCG device for ≈5 h (4.5 Hz). As shown

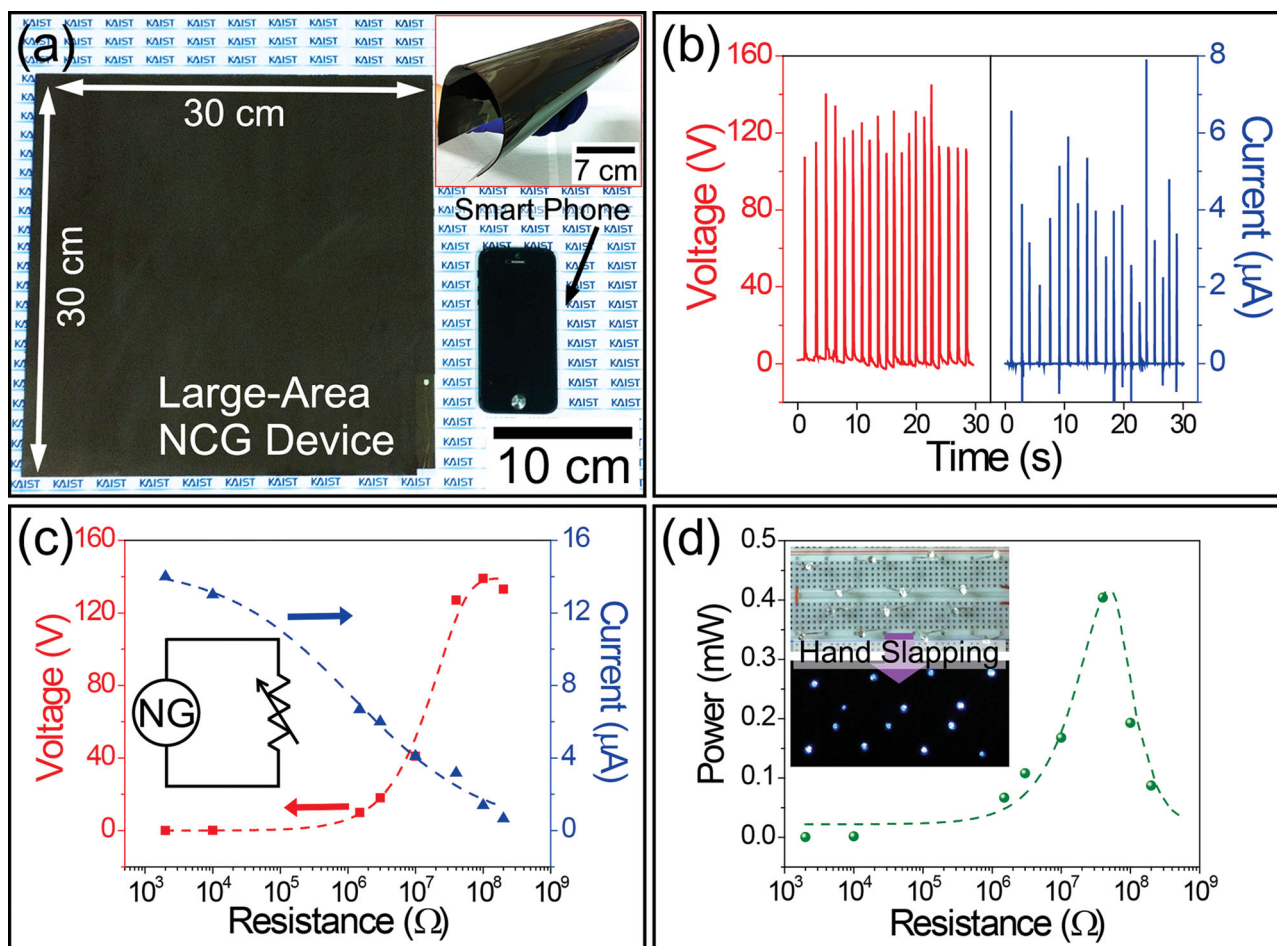


Figure 6. a) Digital photograph of KNLN-based large-area NCG device (30 cm × 30 cm) fabricated by a bar-coating method. The inset shows the rollability of the large-area NCG device. b) The generated output voltage and current signals from the NCG device, with forward connection of measurement unit, during the irregular mechanical impact by hand clapping. c) Dependence of the voltage and current output signals on the outer variable resistance. d) Instantaneous power outputs as a function of the load resistance, which are calculated by $W = V^2 R^{-1}$ where W , V , and R are power, voltage and resistance, respectively. The inset shows an array of 14 blue LEDs in series simultaneously turned on by the electricity generated from the large-area NCG device with no external circuit.

the bottom inset of Figure 5d, the total stored voltage in three capacitors reaches up to 12.55 V. Finally, a super twisted nematic (STN) LCD device is incorporated in circuits with a metal-patterned text mask (top inset of Figure 5d), and successfully operated by the stored electrical energy (see Figure 5d and Supporting Information Video S1).

This lead-free NCG technology can be used to realize a large-area energy harvesting device using the simple and economical process of bar-coating.^[41,42] Figure 6a shows a large-area (30 cm × 30 cm) KNLN-based NCG device; which is wider than the area of thirteen smart phones. This large-area NCG, impacted by clapping, is able to generate a maximum open-circuit voltage of ≈140 V and a short-circuit current of ≈8 μA (Figure 6b). The deviation and one-side polarity of the output peaks are caused by the weak mechanical effect of hand-raising and the irregularity of impact area. The output results of reverse connection with a measurement unit are presented in Figure S8 (Supporting Information). The voltage signals through the outer resistor gradually rise with increasing resist-

ance, and saturated at infinitely high resistance like the open-circuit voltage (Figure 6c). In contrast, the current signals across the variant load decrease from the saturated short-circuit current when the resistance increases. The calculated instantaneous power on the outer load by the large-area KNLN-based nanogenerator reaches up to the maximum value of about 0.5 mW at a resistance of ≈40 MΩ, as shown in Figure 6d. The electricity generated from these biomechanical agitations is used to directly operate 14 blue LEDs in serial connection without any capacitors or batteries (inset of Figure 6d). These results demonstrate that energy harvesting technology using NCG devices with KNLN particles and Cu NRs can successfully drive commercial electronic units.

3. Conclusions

In summary, a high-performance and lead-free NCG device incorporating the piezoelectric KNLN particles and the

well-dispersible Cu NRs has been demonstrated. The flexible NCG device can generate remarkable electrical outputs by the bending or hand tapping due to the outstanding piezoelectric properties of the KNLN. A large-area NCG device fabricated by the bar-coating technique is able to generate \sim mW power (\approx 140 V and \approx 8 μ A) from biomechanical energy. The KNLN-based NCG device exhibits outstanding stability and robustness without any degradation. The electrical power converted by the NCG is used to directly turn on 14 commercial LEDs with no external energy source. The KNLN-based NCG using Cu NRs filler creates higher electrical outputs than any other flexible and lead-free composite-based nanogenerators previously reported. In addition, the effective energy harvesting of our KNLN/Cu NRs NCG system is thoroughly verified by the FEM simulation and theoretical approach. Our high-output and lead-free NCG technology is a crucial improvement in the research for self-powered flexible energy source to achieve the bio-eco-compatible flexible electronics and sensor network in ubiquitous wireless communication. Moreover, through the simple coating methods using bars or roller machines, we are currently developing the NCG-based on-road energy harvesting systems which can be economically realized without complicated vacuum and semiconductor processing.

4. Experimental Section

Preparation of KNLN Particles: Reagent grade of K_2CO_3 (>99%), Na_2CO_3 (>99.5%), Nb_2O_5 (>99.9%), and Li_2CO_3 (>99%) (All from Sigma-Aldrich) were used to prepare the $0.942(K_{0.480}Na_{0.535})NbO_3 \cdot 0.058LiNbO_3$ (KNLN). This nominal composition was selected due to its high piezoelectric voltage coefficient (g_{ij}) at room temperature as reported in the literature.^[21,22] Before mixing the powders, they were dried at the oven for more than 1 week. The raw powder mixture of K_2CO_3 , Na_2CO_3 , Nb_2O_5 , and Li_2CO_3 was ball-milled using high purity 3Y-TZP (Tetragonal Zirconia Polycrystalline) ball media and ethanol in a polyethylene jar for 24 h. The mixed slurry was vacuum-dried and calcined for 4 h in a high purity alumina crucible for KNLN phase formation at 750 °C. After crushing and sieving the calcined powder by #100 standard mesh, the secondary calcination process was performed at 1050 °C for 2 h to obtain high piezoelectric properties by typical sintering effects in KNLN ceramics. Some calcined coarse KNLN lumps were crushed by ball-milling for 5 h for appropriate micron-size powder prior to fabrication of NCG devices.

Material Characterizations: The crystallinity of the KNLN particles and Cu NRs was investigated by X-ray diffraction (XRD, Rigaku, D/MAX-2500, Tokyo, Japan) using $CuK\alpha$ radiation. High-resolution dispersive Raman microscope (ARAMIS, Horiba Jobin Yvon, France) was used to characterize the KNLN particles using a 514.5 nm Ar^+ laser source. Scanning electron microscope (SEM, S-4800, Hitachi, Japan) and field emission transmission electron microscope (FE-TEM 300 kV, Tecnai G2 F30, FEI Co., USA) were utilized to examine the morphologies and the crystal structure of nanomaterials, respectively.

Fabrication Steps for the NCG Devices: To produce the p-NC, KNLN particles (2 g) and Cu NRs (1 g, Sky Spring Nanomaterials, Inc.) were initially mixed in ethanol (OCI Co., Ltd.) using magnetic stirring (650 rpm) for 3 h. After drying and granulating the mixed nanomaterials, the fluidic PDMS (Sylgard 184, Dow Corning, base and curing agent at ratio of 10:1) was blended with the mixture for the final p-NC. The PDMS/p-NC/PDMS fluids were sequentially spin-casted onto a glass plate and cured at 70 °C for 3 min in an oven. Then, this semi-cured three-layered film was sandwiched between an ITO-coated thin PET film (50 μ m in thickness, SKC) and a thick PET substrate (175 μ m in thickness, Sigma-Aldrich). After fully hardening this final NCG device

for 1 day, Cu wires were connected to the ITO electrodes by conductive epoxy (Chemtronics). The finished NCG device was poled overnight at 150 °C with an applied voltage of 2 kV.

Fabrication Steps for the Large-Area NCG Device: The PDMS layer was coated on the ITO-deposited PET substrate (30 cm \times 30 cm, Sigma-Aldrich) using a bar-coater (D-Bar of No.120 μ m, OSG Co.) and cured at 85 °C for 10 min in a convection oven. The p-NC layer was subsequently casted onto the PDMS-coated ITO/PET substrates by the same bar-coater. Next, the semi-cured p-NC/PDMS/ITO/PET substrate was attached to a PDMS-coated ITO/PET film. After overnight curing, Cu wires were attached to the ITO electrodes followed by 2 kV poling process at 150 °C for 12 h.

Measurement of Output Signals: To measure the electrical signals generated by the NCG devices during repeated bending and unbending motions, a custom-designed linear motor stage was used for a maximum displacement of 5 mm; at a rate of 0.2 m s⁻¹. To exclude any external effects, the measurement was performed in a Faraday cage on an optical table. The open-circuit voltage and short-circuit current generated by the deformation of the NCG devices were recorded by a Keithley 2612A.

Supporting Information

Supporting Information is available from the Wiley Online Library or from the author.

Acknowledgements

C.K.J. and K.-I.P. contributed equally to this work. This work was supported by the Basic Science Research Program (grant code: NRF-2012R1A2A1A03010415) and Pioneer Research Center Program (NRF-2013M3C1A3042085) funded by the Korea government (MSIP) through the National Research Foundation of Korea (NRF), and the Center for Integrated Smart Sensors funded by the Ministry of Science, ICT & Future Planning as Global Frontier Project (CISS-2012M3A6A6054187). The work was also supported by NRF grant by MSIP (NRF-2012R1A1A2A10041947).

Received: October 10, 2013

Revised: November 16, 2013

Published online: January 7, 2014

- [1] Z. L. Wang, W. Z. Wu, *Angew. Chem. Int. Ed.* **2012**, *51*, 11700.
- [2] S. Xu, Y. Qin, C. Xu, Y. G. Wei, R. S. Yang, Z. L. Wang, *Nat. Nanotechnol.* **2010**, *5*, 366.
- [3] S. Y. Chung, S. Kim, J. H. Lee, K. Kim, S. W. Kim, C. Y. Kang, S. J. Yoon, Y. S. Kim, *Adv. Mater.* **2012**, *24*, 6022.
- [4] Z. L. Wang, J. H. Song, *Science* **2006**, *312*, 242.
- [5] X. D. Wang, J. Liu, J. H. Song, Z. L. Wang, *Nano Lett.* **2007**, *7*, 2475.
- [6] C. F. Pan, Z. T. Li, W. X. Guo, J. Zhu, Z. L. Wang, *Angew. Chem. Int. Ed.* **2011**, *50*, 11192.
- [7] Z. L. Wang, G. Zhu, Y. Yang, S. H. Wang, C. F. Pan, *Mater. Today* **2012**, *15*, 532.
- [8] K. I. Park, M. Lee, Y. Liu, S. Moon, G. T. Hwang, G. Zhu, J. E. Kim, S. O. Kim, D. K. Kim, Z. L. Wang, K. J. Lee, *Adv. Mater.* **2012**, *24*, 2999.
- [9] K. Tanaka, K. Suzuki, K. Nishizawa, T. Miki, K. Kato, *Jpn. J. Appl. Phys.* **2005**, *44*, 6885.
- [10] H. Maiwa, N. Iizawa, D. Togawa, T. Hayashi, W. Sakamoto, M. Yamada, S. Hirano, *Appl. Phys. Lett.* **2003**, *82*, 1760.
- [11] A. L. Holkin, K. G. Brooks, N. Setter, *Appl. Phys. Lett.* **1997**, *71*, 2044.

- [12] Y. Nakashima, W. Sakamoto, H. Maiwa, T. Shimura, T. Yogo, *Jpn. J. Appl. Phys.* **2007**, *46*, L311.
- [13] Y. Saito, H. Takao, T. Tani, T. Nonoyama, K. Takatori, T. Homma, T. Nagaya, M. Nakamura, *Nature* **2004**, *432*, 84.
- [14] Y. P. Guo, K. Kakimoto, H. Ohsato, *Appl. Phys. Lett.* **2004**, *85*, 4121.
- [15] F. Rubio-Marcos, J. J. Romero, D. A. Ochoa, J. E. Garcia, R. Perez, J. F. Fernandez, *J. Am. Ceram. Soc.* **2010**, *93*, 318.
- [16] K. I. Park, S. Xu, Y. Liu, G. T. Hwang, S. J. L. Kang, Z. L. Wang, K. J. Lee, *Nano Lett.* **2010**, *10*, 4939.
- [17] J. H. Jung, C. Y. Chen, B. K. Yun, N. Lee, Y. S. Zhou, W. Jo, L. J. Chou, Z. L. Wang, *Nanotechnology* **2012**, *23*, 375401.
- [18] J. H. Jung, M. Lee, J. I. Hong, Y. Ding, C. Y. Chen, L. J. Chou, Z. L. Wang, *ACS Nano* **2011**, *5*, 10041.
- [19] T. R. Shrout, S. J. Zhang, *J. Electroceram.* **2007**, *19*, 111.
- [20] J. Ryu, J. J. Choi, B. D. Hahn, D. S. Park, W. H. Yoon, K. H. Kim, *Appl. Phys. Lett.* **2007**, *90*, 152901.
- [21] P. Zhao, B. P. Zhang, J. F. Li, *Appl. Phys. Lett.* **2007**, *90*, 242909.
- [22] K. Wang, J. F. Li, N. Liu, *Appl. Phys. Lett.* **2008**, *93*, 092904.
- [23] K. Keshoju, L. Sun, *J. Appl. Phys.* **2009**, *105*, 023515.
- [24] K. Wang, J. F. Li, *Appl. Phys. Lett.* **2007**, *91*, 262902.
- [25] Y. Qi, C. McAlpine, *Energy Environ. Sci.* **2010**, *3*, 1275.
- [26] R. A. Islam, S. Priya, *Appl. Phys. Lett.* **2006**, *88*, 032903.
- [27] K. Shibata, K. Suenaga, A. Nomoto, T. Mishima, *Jpn. J. Appl. Phys.* **2009**, *48*, 121408.
- [28] S. J. Zhang, R. Xia, T. R. Shrout, G. Z. Zang, J. F. Wang, *J. Appl. Phys.* **2006**, *100*, 104108.
- [29] Y. Wakasa, I. Kanno, R. Yokokawa, H. Kotera, K. Shibata, T. Mishima, *Sens. Actuators A* **2011**, *171*, 223.
- [30] D. Berlincourt, in *Ultrasonic Transducer Materials: Chap. 2. Piezoelectric Crystals and Ceramics* (Ed.: O. E. Mattiat), Plenum Press, New York **1971**, 63.
- [31] N. Klein, E. Hollenstein, D. Damjanovic, H. J. Trodahl, N. Setter, M. Kuball, *J. Appl. Phys.* **2007**, *102*, 014112.
- [32] Z. Wang, H. S. Gu, Y. M. Hu, K. Yang, M. Z. Hu, D. Zhou, J. G. Guan, *CrystEngComm* **2010**, *12*, 3157.
- [33] Z. H. Lin, Y. Yang, J. M. Wu, Y. Liu, F. Zhang, Z. L. Wang, *J. Phys. Chem. Lett.* **2012**, *3*, 3599.
- [34] H. Sun, H. Tian, Y. Yang, D. Xie, Y. C. Zhang, X. Liu, S. Ma, H. M. Zhao, T. L. Ren, *Nanoscale* **2013**, *5*, 6117.
- [35] K. Y. Lee, D. Kim, J. H. Lee, T. Y. Kim, M. K. Gupta, S. W. Kim, *Adv. Funct. Mater.* **2013**, DOI: 10.1002/adfm.201301379.
- [36] M. J. O'Connell, S. M. Bachilo, C. B. Huffman, V. C. Moore, M. S. Strano, E. H. Haroz, K. L. Rialon, P. J. Boul, W. H. Noon, C. Kittrell, J. P. Ma, R. H. Hauge, R. B. Weisman, R. E. Smalley, *Science* **2002**, *297*, 593.
- [37] L. Henrard, E. Hernandez, P. Bernier, A. Rubio, *Phys. Rev. B* **1999**, *60*, R8521.
- [38] L. A. Girifalco, M. Hodak, R. S. Lee, *Phys. Rev. B* **2000**, *62*, 13104.
- [39] H. Hammami, M. Arous, M. Lagache, A. Kallel, *J. Alloy. Compd.* **2007**, *430*, 1.
- [40] M. Arous, H. Hammami, M. Lagache, A. Kallel, *J. Non-Cryst. Solids* **2007**, *353*, 4428.
- [41] K. I. Park, C. K. Jeong, J. Ryu, G. T. Hwang, K. J. Lee, *Adv. Energy Mater.* **2013**, *3*, 1539.
- [42] D. Khim, H. Han, K. J. Baeg, J. Kim, S. W. Kwak, D. Y. Kim, Y. Y. Noh, *Adv. Mater.* **2013**, *25*, 4302.